

No. 10-02-01-41R/01

SYSTEM: CRITICALITY CATEGORY: Space Shuttle RSRM 10 1R SUBSYSTEM: Nozzle Subsystem 10-02 PART NAME: Fixed Housing-to-Aft End Ring Joint, ASSEMBLY: 10-02-01 Primary O-ring, Secondary O-ring (2) 10-02-01-41R Rev M PART NO.: (See Section 6.0) FMEA ITEM NO.: CIL REV NO.: M (DCN-533) Boost (BT) PHASE(S): DATE: 10 Apr 2002 QUANTITY: (See Section 6.0) SUPERSEDES PAGE: 341-1ff. EFFECTIVITY: (See Table 101-6) 31 Jul 2000 HAZARD REF.: BN-03 DATED: CIL ANALYST: B. A. Frandsen APPROVED BY: DATE: RELIABILITY ENGINEERING: K. G. Sanofsky 10 Apr 2002 B. H. Prescott 10 Apr 2002 ENGINEERING: 1.0 FAILURE CONDITION: Failure during operation (D) 1.0 Leakage of primary O-ring and secondary O-ring 2.0 FAILURE MODE: 3.0 FAILURE EFFECTS: Failure could result in hot gas flowing through the joint resulting in burn-through and loss of nozzle causing a thrust imbalance between SRBs, loss of RSRM, SRB, crew, and vehicle 4.0 FAILURE CAUSE (FC): FC NO. DESCRIPTION FAILURE CAUSE KEY 1.1 Nonconforming O-ring splice or repair Α 1.2 Nonconforming O-ring dimensions В С 1.3 O-ring cut or damaged 1.4 Nonconforming O-ring voids, inclusions, or subsurface indications D 1.5 Age degradation of O-ring Ε 1.6 Moisture and/or fungus degradation of O-ring F 1.7 O-ring gland does not meet dimensional or surface finish requirements G 1.8 O-ring improperly installed Н 1.9 Transportation, handling, or assembly damage 1.10 Sealing surfaces contamination or corrosion 1.11 Nonconforming physical or mechanical properties Κ



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### 5.0 REDUNDANCY SCREENS:

SCREEN A: Fail--The leak test procedure verifies the secondary O-ring seal. The primary O-ring cannot be

verified due to blockage of potential leak path by sealant.

SCREEN B: Fail--No provision is made for failure detection by the crew

SCREEN C: Fail--The primary and secondary O-ring seal can be lost due to a single credible cause such as a

surface defect on the sealing surface.

The primary O-ring and secondary O-ring, together, form part of a redundant seal system at the fixed housing-to-aft end ring joint when the leak check port seals. The secondary O-ring will see no pressure unless the primary O-ring fails. If the primary O-ring fails, the secondary O-ring will be pressurized and still maintain a seal. If both the primary O-ring and secondary O-ring fail, a leak path will exist and could result in loss of crew and vehicle.

## 6.0 ITEM DESCRIPTION:

The fixed housing-to aft end ring joint has a primary O-ring and secondary O-ring. The joint is assembled per engineering drawings (Figures 1 and 2). Materials are listed in Table 1.

TABLE 1. MATERIALS

===	Drawing No.	Name	======================================	Specification	Quantity
	1U79153	Nose-Throat-Bearing-Cowl Housing Assembly, Nozzle			1/motor
	1U75150	Packing, Preformed Fluorocarbon	Black Fluorocarbon Rubber	STW4-3339	1/motor
	1U52833	Aft End Ring			1/motor
		Corrosion-Preventive Compound and O-ring Lubricant	Heavy-Duty Calcium Grease	STW5-2942	A/R
	1U51916	Cartridge Assembly	Heavy-Duty Calcium Grease, Filtered and Loaded in an Application Cartridge	STW7-3657	A/R
	1U52945	Housing, Nozzle-Fixed			1/motor

## 6.1 CHARACTERISTICS:

- The fixed nozzle housing-to-aft end ring joint allows the fixed housing to be mounted to the aft end ring. The unit is assembled with O-rings and bolts (with Stat-O-Seals and washers) to assure there is no leakage after assembly.
- Primary and secondary O-rings at the nozzle housing-to-aft end ring joint are designed so they maintain constant contact with its cavity at all times. Squeeze, fill, and tracking are taken into account relating to O-ring groove tolerance.
- The joint and seals are an important part of the assembled rocket motor case. The assembled RSRM is a combustion chamber made up of segments and the nozzle, sealed with O-rings, which must contain and direct pressure generated by burning propellant.
- The O-ring is a one-time-use item.

## 7.0 FAILURE HISTORY/RELATED EXPERIENCE:

Current data on test failures, flight failures, unexplained failures, and other failures during RSRM ground processing activity can be found in the PRACA Database.

8.0 OPERATIONAL USE: N/A



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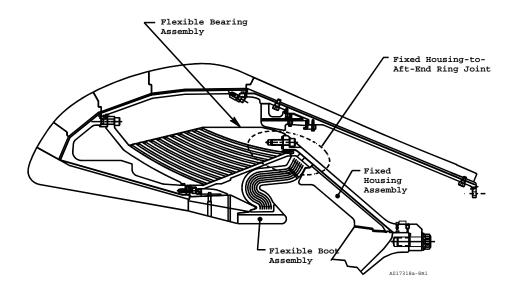


Figure 1. Fixed Housing-to-Aft End Ring Joint Location



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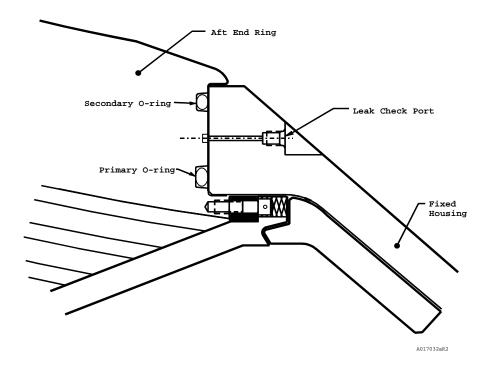


Figure 2. Fixed Housing-to-Aft End Ring Joint



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## 9.0 RATIONALE FOR RETENTION:

## 9.1 DESIGN:

## DCN FAILURE CAUSES

<u>CN</u>	FAILURE CAUSES		
	Α	1.	Large O-rings are per engineering that covers process controls for fabrication of spliced joints and repairs.
	A	2.	Splice joints are cut on an angle and bonded together in a mold (using 100 percent of the scarf area) using an adhesive with the same physical and chemical properties as the parent stock.
	A,D	3.	O-rings were tested to determine size and types of flaws that could cause sealing problems per TWR-17750 and TWR-17991.
	В	4.	Criteria determining O-ring dimensions are per TWR-15771.
	В	5.	Both O-ring designs provide constant contact between the O-ring and mating nozzle sealing surfaces.
	B,D	6.	Large O-rings are per engineering that establishes geometric dimensions, design requirements, and fabrication details.
	С,Н	7.	Large O-rings are individually packaged per engineering.
	C,H	8.	Large O-ring design allows for a minimum of stretching during installation without damage to the O-ring per engineering.
	С	9.	Material selection for O-rings was based in part on resistance to damage per TWR-17082.
	C,H	10.	Design development testing of O-ring twisting and its effect on performance is per ETP-0153 and TWR-17991.
	E	11.	Fluorocarbon rubber O-rings are suitable for periods of storage of up to 20 years (O-ring Handbook, ORD 5700, Copyright 1982, by Parker Seal Group, Lexington, KY). Environment and age are significant to useful seal life, both in storage and actual service as follows:
			<ul> <li>O-rings are packaged and stored to preclude deterioration caused by ozone, grease, ultraviolet light, and excessive temperature.</li> </ul>
	E	12.	Large O-ring time duration of supplier storage and total shelf life prior to installation is per engineering.
	E	13.	Aging studies of O-rings after 5 years installation life were performed. Test results are also applicable to all RSRM fluorocarbon seals. Fluorocarbon maintained its tracking ability and resiliency. Fluorocarbon was certified to maintain its sealing capability over 5 years per TWR-65546.
	E	14.	O-rings are one-time-use items.
	E	15.	Grease is stored at warehouse-ambient condition that is any condition of temperature and relative humidity experienced by the material when stored in an enclosed warehouse, in unopened containers or containers that were resealed after each use. Storage life under these conditions is per engineering.



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		No. 10-02-01-41R/01	DATE: SUPERSEDES PAGE: DATED:	10 Apr 2002 341-1ff. 31 Jul 2000	
E	16.	Aging studies to demonstrate characteristics of grease after 5 years installation life were performed on TEM-9. Results showed that grease provided adequate corrosion protection for D6AC steel, and that all chemical properties of the grease remained intact per TWR-61408 and TWR-64397.		ed adequate	
Е	17.	Large O-rings and filtered grease are included in the	e aft segment life ve	erification.	
F	18.	Large O-rings are black fluorocarbon rubber.			
F	19.	O-ring swell is negligible unless the O-ring und immersion (O-ring Handbook, ORD 5700, Copyrig Lexington, KY).			
F	20.		Fluorocarbon rubber is a non-nutrient to fungus growth (O-ring Handbook, ORD 5700, Copyright 1982, by Parker Seal Group, Lexington, KY).		
F	21.	Large O-rings are kept dry and clean prior to packa	ging.		
G	22.	O-ring gland design is per engineering drawing determined by Thiokol Design Engineering calcuracking per TWR-15771.			
G	23.	Design verification analysis of data from live firing 17563 shows that O-ring sealing surfaces are acce 09.	tests per TWR-1653 ptable for flight per	4 and TWR- TWR-18764-	
G	24.	Sealing surface requirements during refurbishmentand specifications.	nt are per engineeri	ng drawings	
1	25.	Transportation and handling of nozzle assembly ite	ms by Thiokol is per	IHM 29.	
I	26.	The RSRM and its component parts, when protect 11325, are capable of being handled and trans means to and from fabrication, test, operational larefurbishment sites.	ported by rail or of	ther suitable	
I	27.	Positive cradling or support devices and tie dow weight, and contour of components to be trans RSRM segments and other components. Shock devices are used on trucks and dollies to move ser	ported are provided mounting and other	to support er protective	
1	28.	Support equipment used to test, handle, transport the RSRM is certified and verified per TWR-15723.		disassemble	
I	29.	The nozzle assembly is shipped in the aft segme and vibration levels are monitored per engineering by analysis. Monitoring records are evaluated vibration levels per MSFC specification SE-019-04 16975 documents compliance of the nozzle specifications.	and applicable loads by Thiokol to verify 9-2H were not exce	s are derived shock and eded. TWR-	
I	30.	Analysis is conducted by Thiokol engineering to a response of the RSRM nozzle during transportatio launch sites per TWR-16975.			
J	31.	Filtered grease is applied to sealing surfaces of cowl-housing assembly during final assembly proce		roat-bearing-	



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## CRITICAL ITEMS LIST (CIL)

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J	32.	Filtered grease filtering is per engineering to control	contamination.	
J	33.	Removal of surface contamination or corrosion is whenever contamination or corrosion is noted.	a standard shop pr	ractice used
J	34.	Contamination control requirements and procedures	s are per TWR-1656	4.
К	35.	Large O-rings are high temperature, low compression set, fluid resistant, black fluorocarbon rubber.		
K	36.	Filtered grease is per engineering drawings and material requirements determined by Thiokol engineering.		
Κ	37.	Temperature prior to launch is monitored for the nozzle flexible bearing and the case-to-nozzle joint and is maintained per TWR-15832. The fixed housing-to-aft end ring joint is within the temperature maintained area and benefits from temperature conditioning. Joint thermal analysis (O-ring resiliency testing) is per ETP-0276 and TWR-18597.		
B,G,I	38.	Analysis of carbon-cloth phenolic ply angle changes for the nozzle was performed. Results show that redesigned nozzle phenolic components have a reduced inplane fiber strain and wedge-out potential per TWR-16975. New loads that were driven by the Performance Enhancement (PE) Program were addressed in TWR-73984. No significant effects on the performance of the RSRM nozzle were identified due to PE.		
B,G,I	39.	performance factor equation based on the remainin phase is complete. This performance factor will be safety factor of 1.4 for the fixed housing assembly p 75135. (Carbon phenolic-to-glass interface, bondlin housing temperatures were all taken into considerar factor will insure that the CEI requirements will be m between carbon and glass will not exceed 600 degr	g virgin material afte equal to or greater the TWR-74238 and e temperature and nation). The new performet which requires the E, bondline of gland.	er boost han a TWR- netal rmance at the bond ass-to-
	J J K K K	J 33.  J 34.  K 35.  K 36.  K 37.	No. 10-02-01-41R/01  J 32. Filtered grease filtering is per engineering to control whenever contamination or corrosion is whenever contamination or corrosion is noted.  J 34. Contamination control requirements and procedured fluorocarbon rubber.  K 35. Large O-rings are high temperature, low compress fluorocarbon rubber.  K 36. Filtered grease is per engineering drawings and menome by Thiokol engineering.  K 37. Temperature prior to launch is monitored for the case-to-nozzle joint and is maintained per TWR-1 end ring joint is within the temperature maintagenerature conditioning. Joint thermal analysis of ETP-0276 and TWR-18597.  B,G,I 38. Analysis of carbon-cloth phenolic ply angle change Results show that redesigned nozzle phenolic collaboration per TW driven by the Performance Enhancement (PE) Proceeding the performance factor equation based on the remaining phase is complete. This performance factor will be safety factor of 1.4 for the fixed housing assembly possible factor will insure that the CEI requirements will be not between carbon and glass will not exceed 600 degrine metal remains at ambient temperature during boos	DATE: SUPERSEDES PAGE: DATED:  J 32. Filtered grease filtering is per engineering to control contamination.  J 33. Removal of surface contamination or corrosion is a standard shop provide whenever contamination or corrosion is noted.  J 34. Contamination control requirements and procedures are per TWR-1656.  K 35. Large O-rings are high temperature, low compression set, fluid resifluorocarbon rubber.  K 36. Filtered grease is per engineering drawings and material requirements by Thiokol engineering.  K 37. Temperature prior to launch is monitored for the nozzle flexible bear case-to-nozzle joint and is maintained per TWR-15832. The fixed he end ring joint is within the temperature maintained area and be temperature conditioning. Joint thermal analysis (O-ring resiliency te ETP-0276 and TWR-18597.  B,G,I 38. Analysis of carbon-cloth phenolic ply angle changes for the nozzle was Results show that redesigned nozzle phenolic components have a plane fiber strain and wedge-out potential per TWR-16975. New load driven by the Performance Enhancement (PE) Program were address 73984. No significant effects on the performance of the RSRM ridentified due to PE.  B,G,I 39. Thermal analysis per TWR-17219 shows the nozzle phenolic meets the performance factor equation based on the remaining virgin material afte phase is complete. This performance factor will be equal to or greater to safety factor of 1.4 for the fixed housing assembly per TWR-4238 and 75135. (Carbon phenolic-to-glass interface, bondline temperature and nousing temperatures were all taken into consideration). The new performace factor will be equal to or greater to safety factor of 1.4 for the fixed housing assembly per TWR-4238 and 75135. (Carbon phenolic-to-glass interface, bondline temperature and nousing temperatures were all taken into consideration). The new performace factor will insure that the CEI requirements will be met which requires the between carbon and glass will not exceed 600 degree F, bondline of glass.



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## 9.2 TEST AND INSPECTION

# $\begin{array}{cc} & \text{FAILURE CAUSES and} \\ \underline{\text{DCN}} & \underline{\text{TESTS}} & (\underline{\text{T}}) \end{array}$

CIL CODE

1. For New Large O-ring verify:

A A		a. b.	Diameter Splice is bonded over 100 percent of the scarf	AEB026,AEB027 area AEB133,AEB134
A		C.	No more than five splices	AEB167,AEB169
Α		d.	Repairs	AEB265,AEB266
Α		e.	Adhesive is made from fluorocarbon rubber	AEB308,AEB311
Α		f.	Splice bond integrity	AEB317,AEB319
A,D	(T)	g.	Subsurface indications	AEB354
A,C,D,F		h.	Surface quality	AEB388,AEB389
A,K	(T)	i.	Tensile strength	AEB401,AEB402
A,K	(T)	j.	Ultimate elongation	AEB442,AEB443
В		k.	Diameter	AEB015,AEB014,AEB018,AEB023
В		I.	Correct identification	AEB087,AEB100
C,E,F		m.	Packaging for damage or violation	AEB179
E,F,K		n.	Material is fluorocarbon rubber	AEB141,AEB151
E,F		Ο.	Packaging is free of staples or other objects	LAA054
F		p.	Clean and dry when packaged	AEB031,AEB034
K	(T)	q.	Tensile strength	AEB394,AEB396
K	(T)	r.	Ultimate elongation	AGM408,AGW075
K	(T)	S.	Shore A hardness	AGM304,AGM312
K	(T)	t.	Compression set	AKW006,AKW011

## 2. For New Nose-Throat-Bearing-Cowl Housing Assembly, Nozzle verify:

A,B,C,D,				
G,H,I,J	(T)	a.	Joint seals are pressure tested	ADQ114
Н		b.	Correct identification of primary O-ring at time of installation	ADQ052
Н		C.	Correct identification of secondary O-ring at time of installation	ADQ053
C,H		d.	Installation and fit of secondary O-ring	ADQ077
C,H		e.	Installation and fit of primary O-ring	ADQ079
H,J		f.	Application of filtered grease to Aft End Ring O-ring grooves prior	
			to assembly	ADQ012
H,J		g.	Application of filtered grease to Housing, Nozzle-Fixed forward	
			end sealing surfaces prior to assembly	ADQ015
Н		h.	Application of filtered grease to secondary O-ring prior to assembly	ADQ020
Н		i.	Application of filtered grease to primary O-ring prior to assembly	ADQ021
C,H		j.	Primary and secondary O-ring, are unpackaged, processed, and	
			installed one at a time	ADQ136
С		k.	Secondary O-ring is free from damage prior to installation	ADQ149
С		I.	Primary O-ring is free from damage prior to installation	ADQ159
C,H		m.	Condition of secondary O-ring after installation into O-ring groove	ADQ000A
C,H		n.	Condition of primary O-ring after installation into O-ring groove	ADQ001
E		Ο.	Shelf life of the filtered grease was not exceeded prior to use	LAA049
E		p.	Secondary O-ring shelf life has not expired	ADQ134
E		q.	Primary O-ring shelf life has not expired	ADQ176
E		r.	Secondary O-ring packaging has not been damaged or violated	
			prior to installation	ADQ133
E		S.	Primary O-ring packaging has not been damaged or violated prior	
			to installation	ADQ175
F		t.	Secondary O-ring is free from fungus prior to installation	ADQ122
F		u.	Secondary O-ring is free from moisture prior to installation	ADQ123
F		٧.	Primary O-ring is free from fungus prior to installation	ADQ162



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F		w. Primary O-ring is free from moisture prior to		ADQ163
F F		<ul><li>x. O-ring grooves in the Aft End Ring are free f assembly</li><li>y. O-ring grooves in the Aft End Ring are free f</li></ul>	-	ADQ168
i I		assembly  z. O-ring grooves in Aft End Ring are free from	•	ADQ170 ADQ206
I		<ul> <li>aa. Sealing surfaces on Housing, Nozzle-Fixed from damage prior to assembly</li> </ul>	forward end are free	ADQ207
J		ab. Sealing surfaces on Housing, Nozzle-Fixed from corrosion and contamination prior to as	forward end are free ssembly	ADQ202
J		ac. O-ring grooves in Aft End Ring are free from contamination prior to assembly		ADQ208
	3.	For New Filtered Grease verify:		
E,F,J,K E,F,J,K E,F,J,K E,F,J,K E,F,J,K E,F,J,K E,F,J,K		<ul> <li>a. Grease is received from storage unopened of Shelf life of the grease, prior to filtering</li> <li>c. Contamination</li> <li>d. Grease conforms to specification</li> <li>e. Cartridge conforms to drawing</li> <li>f. Filtered grease is capped and sealed after fig.</li> <li>g. Filtered grease is sent to storage capped an and resealed)</li> </ul>	illing	ACP015 AMB018L ANO064 LAA044 LAA046 LAA047
	4.	For New Grease verify:		LANOUS
E,F,J				ANO015
E,F,K E K (T) K (T)		<ul> <li>a. Material received in closed containers</li> <li>b. Type</li> <li>c. No shipping or handling damage</li> <li>d. Penetration</li> <li>e. Dropping point</li> <li>f. Zinc concentration</li> </ul>		ANO050 ANO058 LAA037 ANO042 LAA038
	5.	For New Aft End Ring verify:		
G G G		<ul><li>b. O-ring groove diameter</li><li>c. O-ring groove surface finish</li></ul>	ADE043,ADE043A,ADE044 ADE045,ADE045A,ADE046 ADE047,ADE047A,ADE048 ADE053,ADE053A,ADE054	3,ADE046A 3,ADE048A
	6.	For Refurbished Aft End Ring verify:		
G		a. O-ring groove surface finish		ADE068
	7.	For New Housing, Nozzle-Fixed verify:		
G		a. Surface finish	LAA1	39,LAA140
	8.	For Refurbished Housing, Nozzle Fixed verify:		
G		a. Surface finish		ADV192
	9.	KSC verifies:		
Е		a. Life requirements for the expected launch so OMRSD File II, Vol III, C00CA0.030	chedule are met per	OMD019

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